

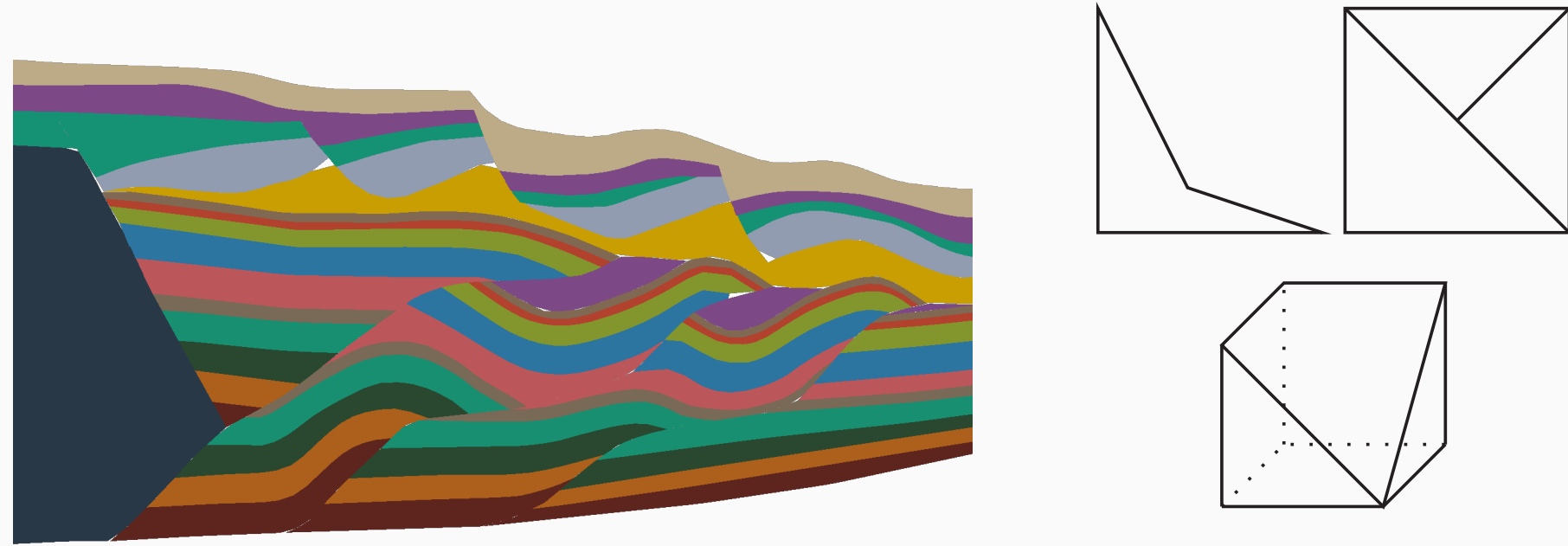
Geomechanics' challenges

Involves two physics

→ Requires two spatial discretization methods working on a **single** mesh

Highly deformed media

→ Methods must work on **poor quality** meshes



Governing equations

Under the assumptions of quasistatic strains and slightly compressible single-phase flow, the mechanical equilibrium and the fluid mass conservation are coupled through Biot's equations.

$$-\text{div}(\bar{\bar{C}}\bar{\bar{\epsilon}}_u - \alpha p \bar{\bar{I}}_d) = \mathbf{f} \quad \text{with } \bar{\bar{\epsilon}}_u = \frac{1}{2}(\nabla \mathbf{u} + \nabla \mathbf{u}^T)$$

$$\partial_t(c_0 p + \alpha \text{div}(\mathbf{u})) + \text{div}(-\bar{\kappa}(\nabla p - \rho_f \mathbf{g})) = q$$

where \mathbf{u} is the solid displacement and p the fluid pressure.

In this work, we assume that the solid has a linear elastic behaviour described by the stiffness tensor $\bar{\bar{C}}$.

α	Biot parameter
c_0	Constrained specific storage coefficient
ρ_f	fluid density
$\bar{\kappa}$	Mobility matrix

Spatial discretization

Working in a **variational** framework for the mechanics and in the **finite volume** framework for the fluid flow,

$$a(\mathbf{u}_h^n, \mathbf{v}_h) - \sum_K \alpha \int_K \text{div}(\mathbf{v}_h) p_h^n = \int_\Omega \mathbf{f}^n \cdot \mathbf{v}_h$$

$$\int_K (c_0 p_h^n + \alpha \text{div}(\mathbf{u}_h^n)) + \Delta t \sum_{f \subset \partial K} \mathcal{F}_{Kf}^n = \int_K (\Delta t q^n + c_0 p_h^{n-1} + \alpha \text{div}(\mathbf{u}_h^{n-1}))$$

Given two bases for the discrete spaces, the equivalent matrix form is given by

$$\begin{bmatrix} \mathcal{A} & -\mathcal{B} \\ \mathcal{B}^T & \mathcal{F} \end{bmatrix} \begin{bmatrix} \mathcal{U} \\ \mathcal{P} \end{bmatrix} = \begin{bmatrix} \mathcal{L}^u \\ \mathcal{L}^p + \mathcal{L}^c \end{bmatrix} \quad \text{where } \mathcal{F} \text{ depends only on flow problem,}$$

\mathcal{A} depends only on the elasticity problem,
 \mathcal{B} stores the coupling terms $\int p_h^n \text{div}(\mathbf{v}_h)$.

We can now choose a discretization method for \mathcal{A} and another for \mathcal{F} . Indeed, the scheme can be customized picking the following elements:

A) A Virtual Element Method

Key idea of VEM[1]: on each element, substitute a with an approximate discrete form a_h

- consistent (ensures accuracy)
- stable (ensures coercivity)
- computable from the *dofs*.

To have the consistency and the stability, set

$$a_h^K(\mathbf{u}, \mathbf{v}) := a^K(\pi^K \mathbf{u}, \pi^K \mathbf{v}) + h_K^{d-2} \max |\bar{\bar{C}}| s^K (\mathbf{u} - \pi^K \mathbf{u}, \mathbf{v} - \pi^K \mathbf{v})$$

where $\pi^K \mathbf{u}$ is a projection to the polynomial part of \mathbf{u} and where s^K stabilizes the non polynomial part. For the lowest order of accuracy, we can take

$$\pi^K \mathbf{v}(\mathbf{x}) = \left(\frac{1}{|K|} \int_K \nabla \mathbf{v} \right) (\mathbf{x} - \bar{\mathbf{x}}_K) + \frac{1}{M_K} \sum_{i \in M_K} \mathbf{v}(V_i)$$

which is computable from the *dofs*. With this approximate form, basis functions are *virtually* defined over any general element.

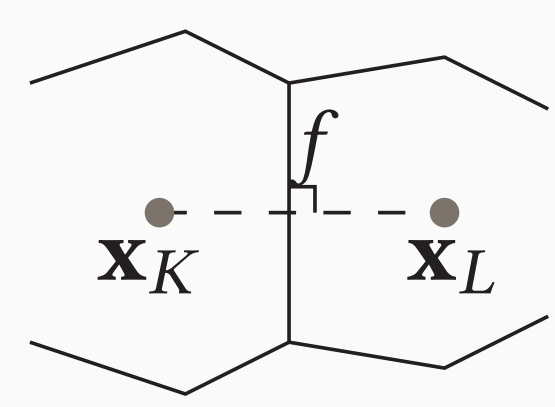
B) A Finite Volume scheme

Choosing any fv scheme with cell-centered unknowns allows an easy treatment of the coupling terms. From [2] we highlight:

▷ *Two-Point Flux Approximation*

Use only two points to compute the fluxes

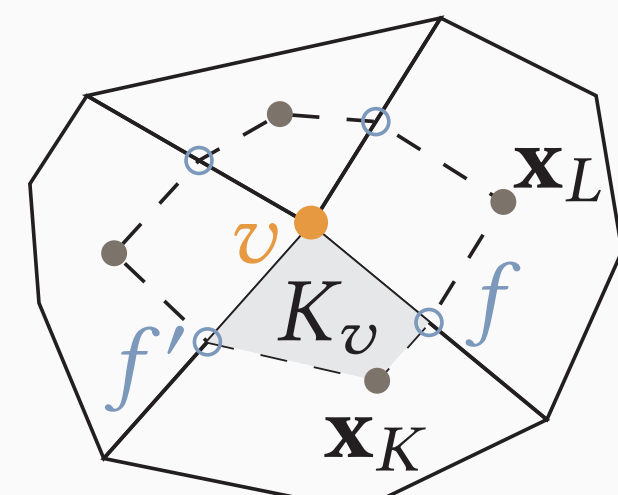
$$\mathcal{F}_{Kf} = |f| \kappa_{KL} d_{KL}^{-1} (p_K - p_L)$$



- ♥ Low computational cost
- ♥ High stability
- ♥ Requires orthogonality condition $(KL) \perp f$

▷ *Multi-Point Flux Approximation*

Compute half fluxes \mathcal{F}_{Kfv} , then eliminate face unknowns using consistency $\mathcal{F}_{Kfv} + \mathcal{F}_{Lfv} = 0$ and finally sum half fluxes to get $\mathcal{F}_{Kf} = \mathcal{F}_{Kfv} + \mathcal{F}_{Kfv}$.



- ♥ Allows more general meshes
- ♥ Larger stencil (more costly)
- ♥ Sometimes unstable

C) A Solution Strategy

Use either a **fully** coupled (monolithic) or an **iteratively** coupled strategy.

▷ *Fully coupled resolution*

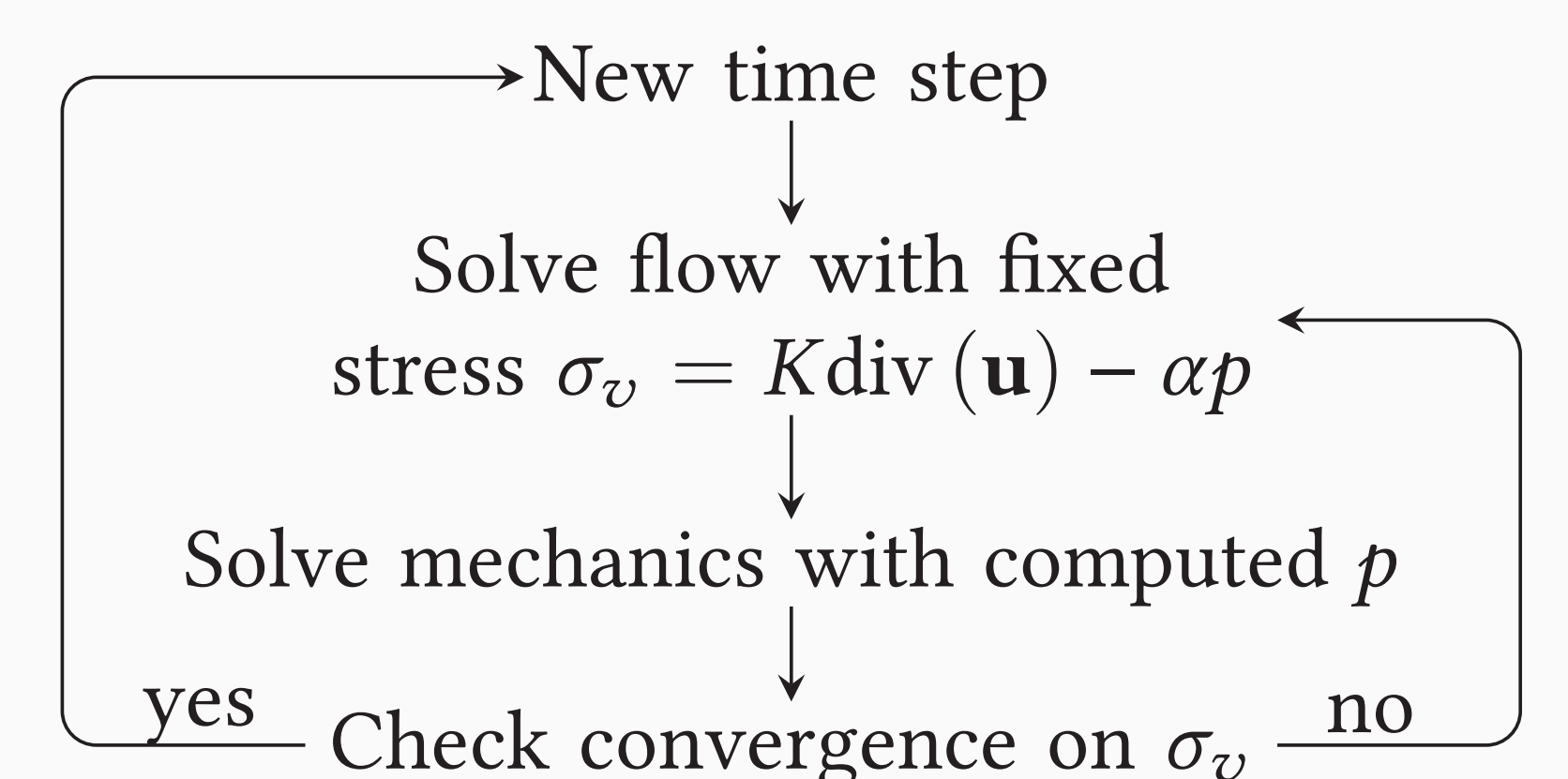
Both equations are simultaneously solved.

♥ Unconditionally stable

♥ Huge matrix, no efficient solver available

▷ *Iteratively coupled resolution*

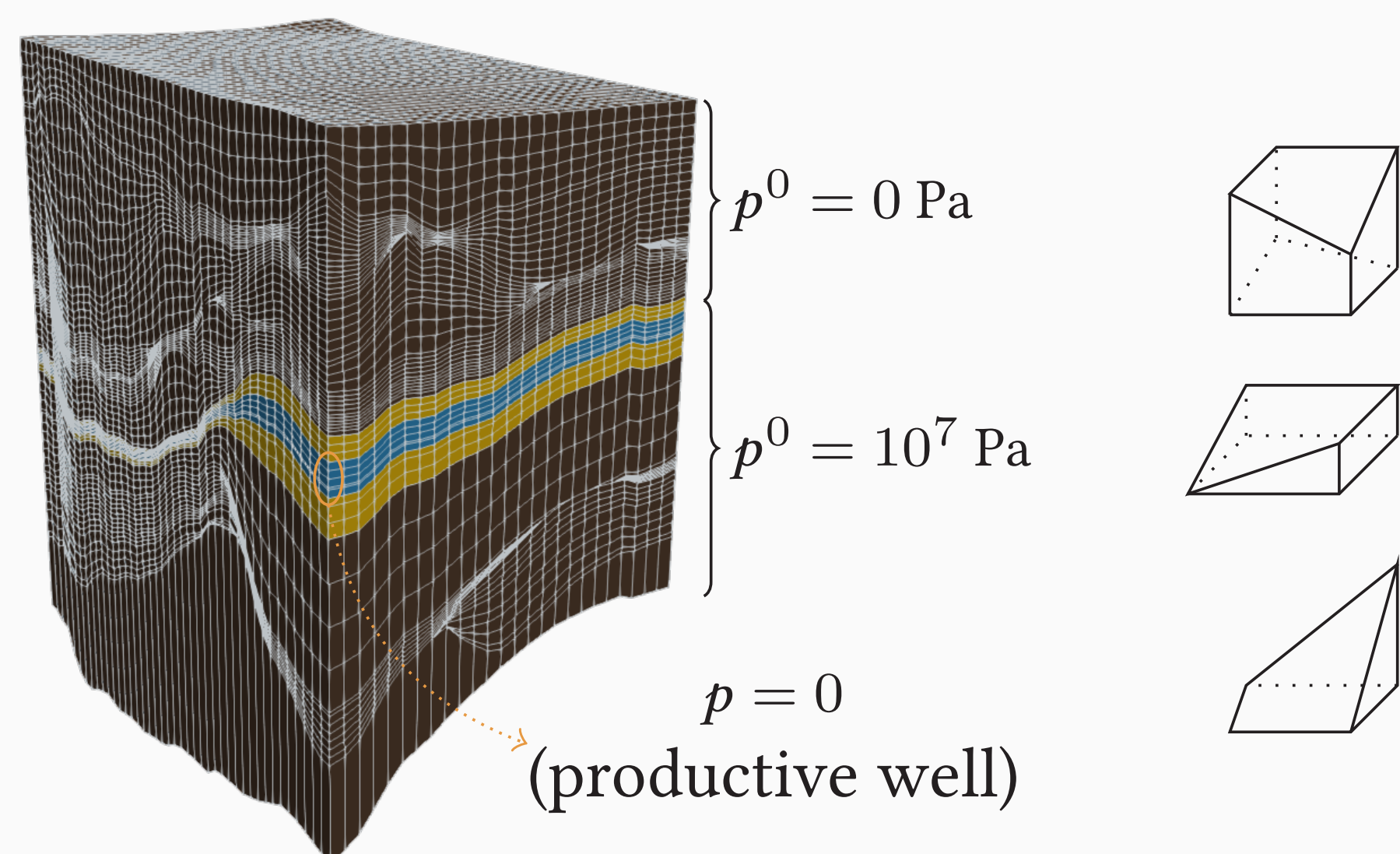
Use a splitting [3] such as the fixed-stress split:



- ♥ More iterations, needs a convergence criteria
- ♥ Pick specialized solvers for each subproblem
- ♥ Krylov-like methods can speed up convergence

Numerical illustration

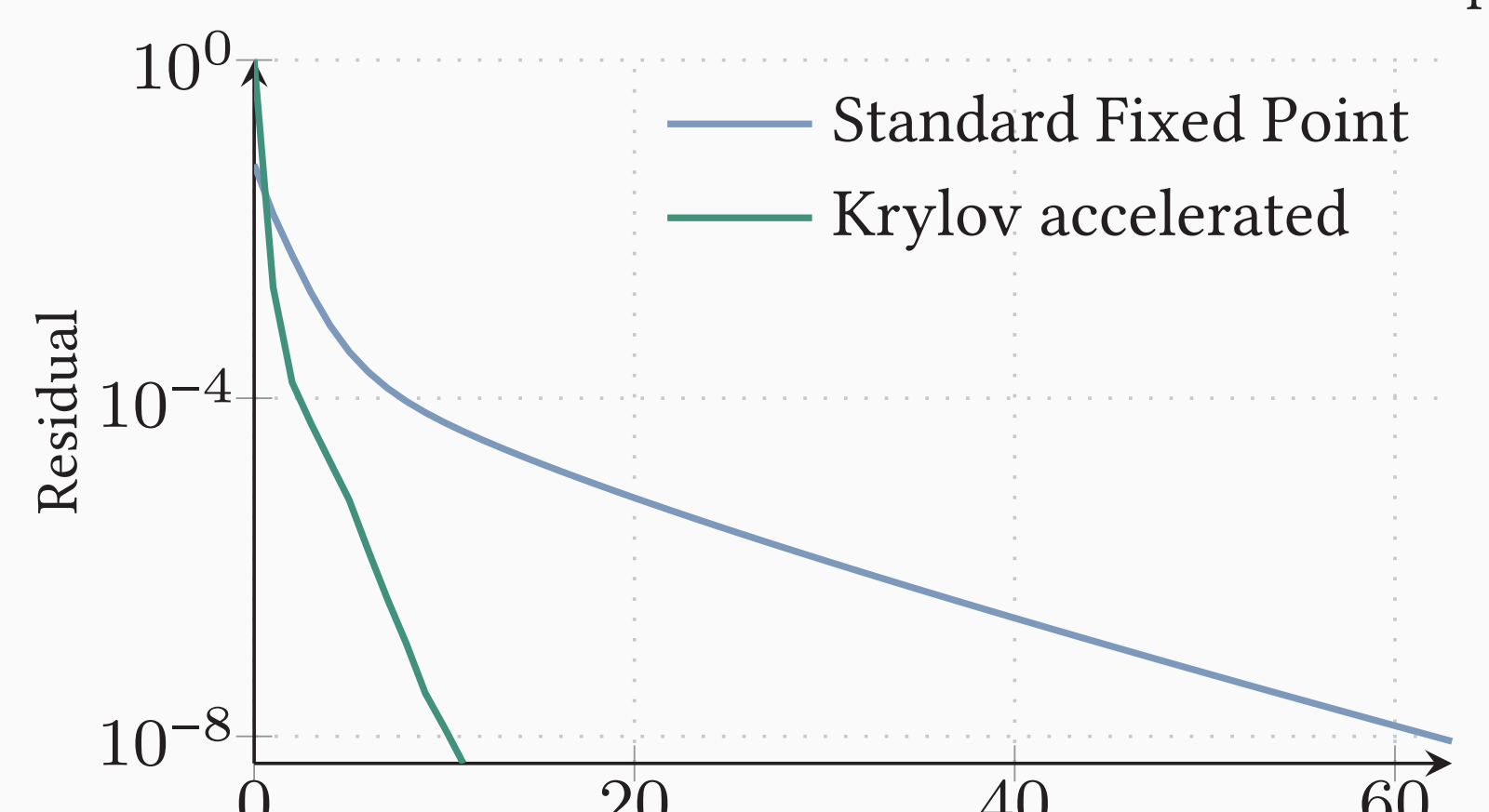
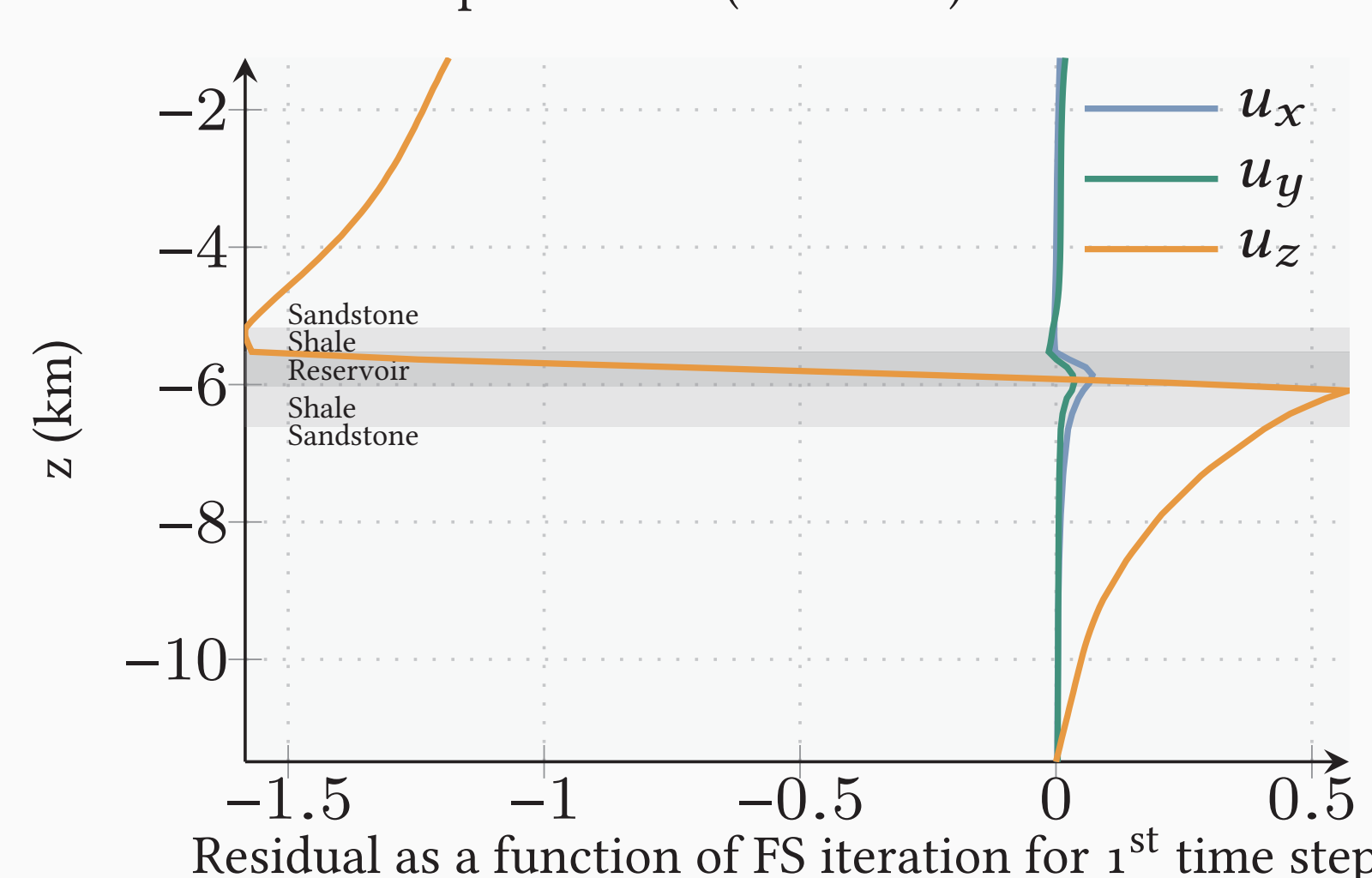
Layered 3D mesh including degenerated cells



	κ	ϕ	E	ν	α
Sandstone	10^{-9}	0.2	$5 \cdot 10^9$	0.3	1
Shale	10^{-15}	0.1	$5 \cdot 10^9$	0.3	1
Reservoir	10^{-9}	0.3	10^9	0.3	1

Bottom and lateral faces: $\nabla p \cdot \mathbf{n} = 0, \mathbf{u} \cdot \mathbf{n} = 0$
Top face: $p = 0$ and free stress condition

→ Solve ~300K dofs over 20 time steps (T=1 year) with **VEM-MPFA** and the **fixed-stress** strategy:
Relative displacements (in meters) over a vertical line



References

- [1] L. Beirão Da Veiga, C. Lovadina, and D. Mora. "A Virtual Element Method for elastic and inelastic problems on polytope meshes". In: *Computer Methods in Applied Mechanics and Engineering* 295 (2015), pp. 327–346.
- [2] J. Droniou. "Finite volume schemes for diffusion equations: Introduction to and review of modern methods". In: *Math. Models & Methods in App. Sciences* 24.8, SI (2014), pp. 1575–1619.
- [3] A. Mikelić, B. Wang, and M. F. Wheeler. "Numerical convergence study of iterative coupling for coupled flow and geomechanics". In: *Comp. Geosciences* 18.3 (2014), pp. 325–341.

Future works

Use domain decomposition methods as an efficient preconditioner to solve \mathbf{u}
More general mechanical laws