



Modelling Geological Nuclear Waste Disposal : Some Thermo-Hydro- Mechanical (THM) problems in porous media

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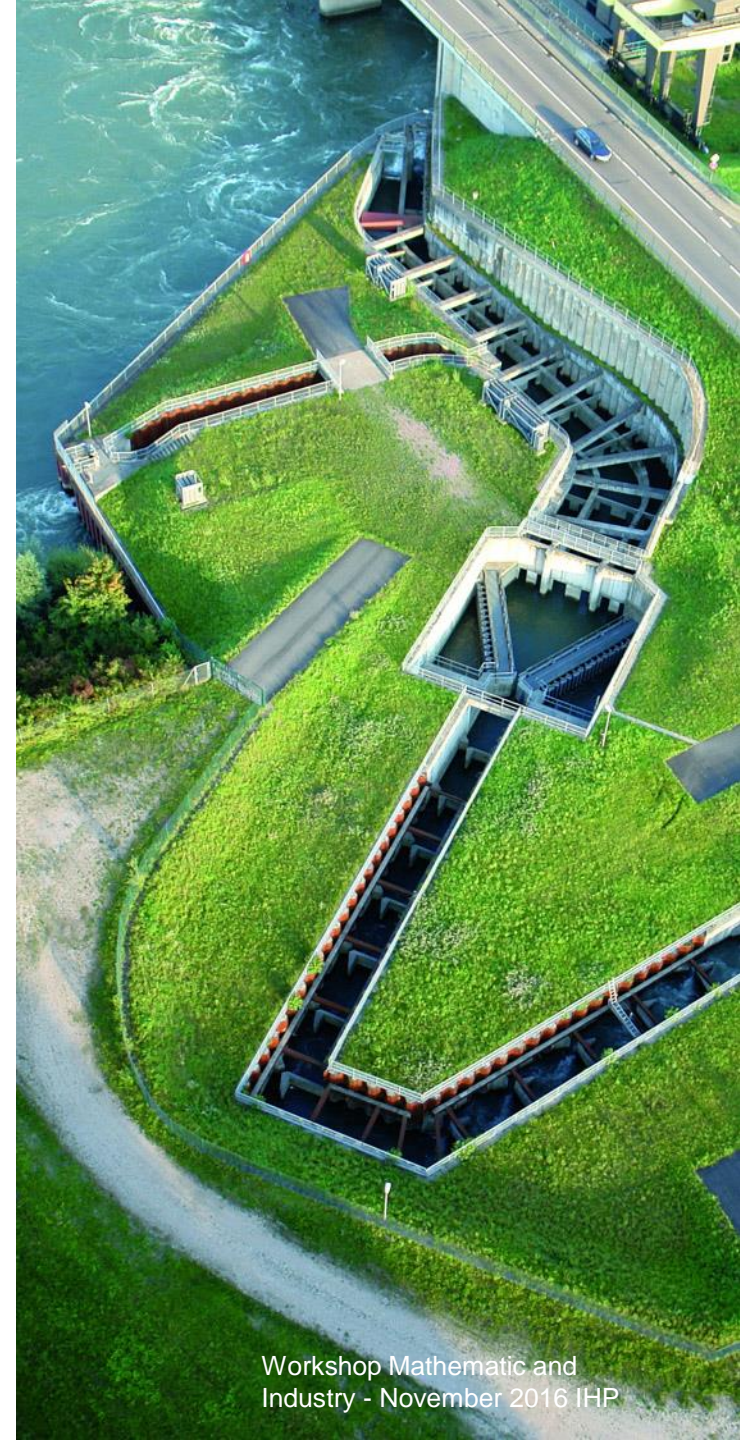
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Outline



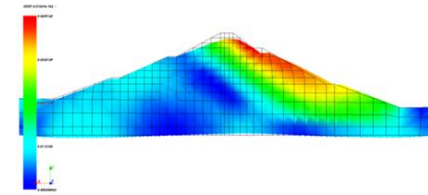
- General Context
- General Macroscopic THM model description
- Examples of THM problems
 - ✓ Mechanical laws and numerical treatments
 - ✓ Simulation of in situ experiment
- Numerical locks and perspectives
- General Conclusions



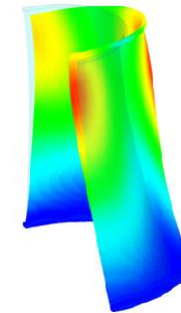
General Context (1/4)

Multiphysic problems in porous media in electricity industry

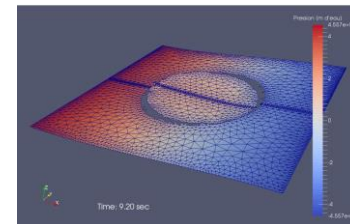
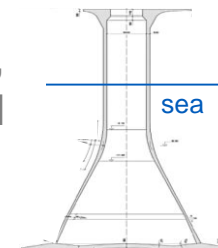
- Hydraulic buildings (dams ...)
 - Coupling between hydraulic and mechanic (impoundment, emptying, level variation)
 - Seismic risk (dynamic problems)



- Containment structures, air coolers
 - Coupling between H, T, and M
 - Estimation of leakage in concrete structures



- Wind turbine
 - Modeling of the ground (flow, overpressure, hydrodynamic loading ...) under a Gravitary Based Structure (BGS)

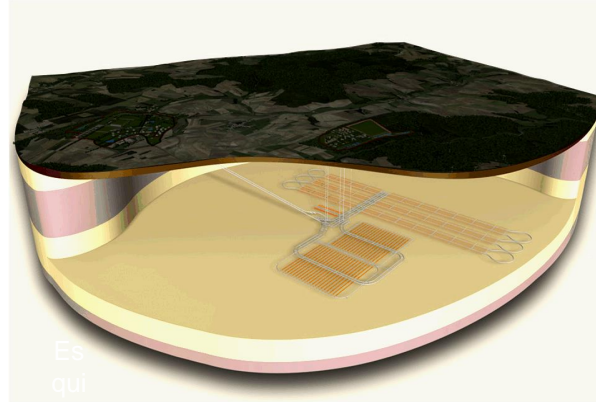


Water Pressure (Flejou 2016)

General Context (2/4)

➤ Nuclear waste disposal (responsible : Andra)

- A network of galleries and cells in Callovo-Oxfordian argillite (- 500 m)



Esquisse Andra

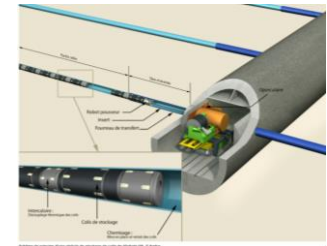
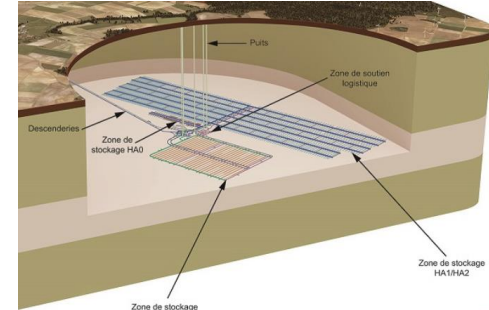
- Robustness and safety
- Dimensioning and optimization of the geometry (compactness of the installations)

General Context (3/4)

Issues for porous media modeling in nuclear waste disposal

- Near Field THM modeling

- Estimation of the Excavation Damage Zone (EDZ) around galleries and cells – Study of the digging
- Study of the concrete → dimensioning of concrete lining
- Understanding and prediction of the comportment of sealings and plugs : swelling and saturation/desaturation mechanisms
- Comportment of voids between materials
- Estimation of temperature and liquid pressure due to thermal dilatation – Mechanical consequences
- Estimation of the Hydrogen pressure (corrosion, radiolysis) and Gas preferential pathways



Esquisse Andra

- Package modeling

- Radiolysis Hydrogen production in cementitious package (surface disposal)
- Bituminous package : risk of swelling under water uptake => THMC problem (multicomponents)



General Context (4/4)

- Specificities

- A fully coupled T.H.M (C) problem (Multiphysic problem)
- A complex geometry : 3D, from cells to geological layer ; crossing of galleries
- Time dependant problem at different scales from tunnel excavation until post-closure stage : evolution of excavation, creeping of host rock, thermal problem, hydrogen production ...
- Heterogeneous materials with high contrasts and specific compartments
 - Intact or damage host rocks, sealing, plugs, concrete, bituminous, steels ...
 - Goal of anisotropy
- High contrast of initial conditions: stiff front
- Hydraulic specificities : low permeability, weak desaturation of host rock, high level of capillary pressure and of water and gas pressure ...

=> Software Code_Aster (www.code_aster.org)

High number of parameters and high number of experimental data =>

Uncertainties management becomes a crucial issue

Basic THM model

- Hypothesis of a classical model (Coussy formulation)

- Anisotropic porous media constituted by 3 phases (compressible liquid + gas + solid) and 2 components (ex. H₂O and H₂)

- Equilibrium equations

- ✓ Mass conservation of each component (classical two-phase flow model)

$$\dot{m}_l^c + \dot{m}_g^c = \text{div}(\mathbf{F}_l^c + \mathbf{F}_g^c) = 0 \quad c = H_2O, H_2$$

- ✓ Mechanical equilibrium (total stresses)

$$\mathbf{Div}(\boldsymbol{\sigma}) + r\mathbf{F}^m = 0$$

- ✓ Energy conservation

- Component laws

- ✓ Darcy law on each phase (liquid and gas)

$$\frac{\mathbf{F}_p}{\rho_p} = \frac{\mathbf{K}^{\text{int}} k_p^{\text{rel}}(S_p)}{\mu_p} (-\nabla p_p + \rho_p \mathbf{g}) \quad p = l, g$$

- ✓ Porosity evolution linked to solid deformation and dilatation

- ✓ Diffusion : Fick's law for each mixture

- ✓ Gas perfect law

- ✓ Dissolution : Henry's law

- ✓ Vaporization

- ✓ Mechanical laws : $\boldsymbol{\sigma}' = f(\boldsymbol{\varepsilon}, \dots)$ several compartment laws adapted to each material (elastic, elastoplastic, viscoplastic, thermo-viscoplastic ...)

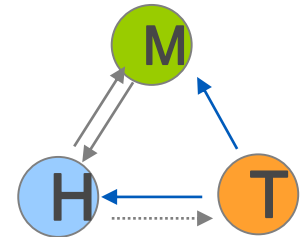
T.H.M couplings description

Mechanic -> Hydraulic

✓ Fully saturated medium : Biot relation

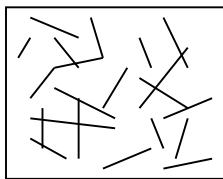
$$\boldsymbol{\sigma} = \boldsymbol{\sigma}' - b p_l \mathbf{I}$$

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}' - b (S_l p_l + S_g p_g) \mathbf{I}$$



Hydraulic -> Mechanical

✓ Permeability affected by damage



—————→
homogenisation

Damage

←————— K

Ex.: $K(\varphi) = f(k_0 \cdot (\varphi - \varphi_0)^3)$

✓ Thermic => Hydraulic : Dilatation of water

✓ Thermic=>Mechanic : Dilatation of skeleton and mechanical stresses due to temperature

✓ Hydraulic=> Thermic: effect of desaturation

General numerical choices

- Fully Coupled formulation T,P,U
 - ✓ Two-phase flow modeling : unknowns adapted to gas appearance/disappearance treatment (Angelini et al. 2010)

$$(P_l, \chi_l^{H_2} = \frac{K_H \rho_l^{H_2}}{M^{H_2}}) \text{ instead of } (P_l, P_g)$$

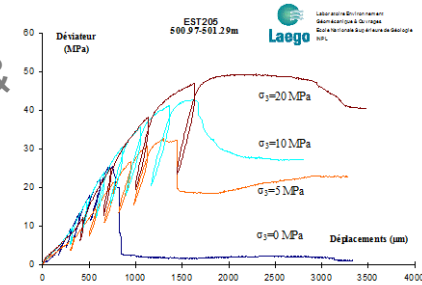
- Finite Elements P2P1 (2D, AXI, 3D) or VF SUSHI for pure hydraulic problems (Angelini et al. 2010)
- Time Euler implicit
- High non linear (S(Pc), kr(S)...) problem solved by Newton Method + Linear research (Newton Krylov available)
- Linear problems solved by direct methods (Mumps) or iterative methods (from PESTC : BCGS, GMRES, etc.)

Mechanical laws and treatment (1/4)

- Mechanical law adapted to material rheology :

➤ For Callovo Oxfordien argilite (ex. L&K, Hoek & Brown...):

- Brittle behavior of the rock
- Softening behavior
- Dilatancy
- Creeping phenomena (viscoplasticity)



Risk : apparition of localization effects due to strong micro deformation gradient not included in classical treatment (only on macroscopic variables)

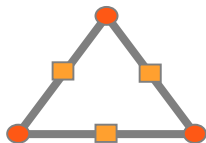
➡ Results are dependent of grid !

Methods of regularization : non local model using a microscopic field

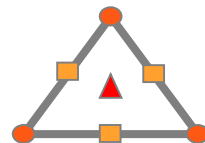
=> Micro Gradient Dilation Model (Fernandes et al. 2009) – regularization only on volumic strain (second gradient)

$$\int_{\Omega} \left(\sigma_{ij} \varepsilon_{ij}^* + D \cdot \frac{\partial \chi}{\partial x_j} \frac{\partial \chi^*}{\partial x_j} \right) d\Omega - \int_{\Omega} \lambda (\varepsilon_v^* - \chi^*) d\Omega = P_e^*$$

$$\int_{\Omega} \lambda^* (\varepsilon_v - \chi) d\Omega = 0 \quad \forall \lambda^* \in L^{ad}$$



● u, p
 ■ u



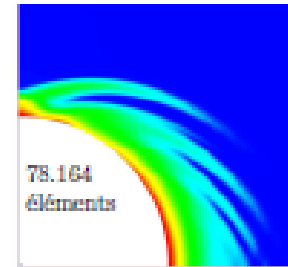
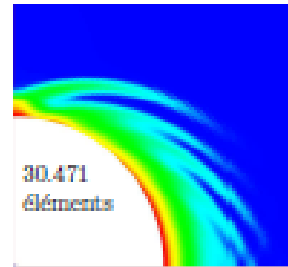
● u, χ, p
 ■ u
 ▲ λ

Mechanical laws and treatment (2/4)

Porosity variation excavation problem without and with second gradient method (from MoMas Benchmark):

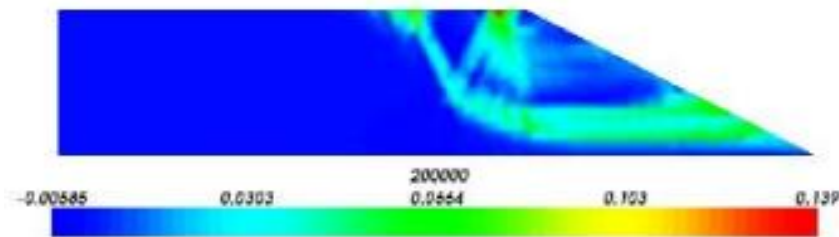


Without regularization

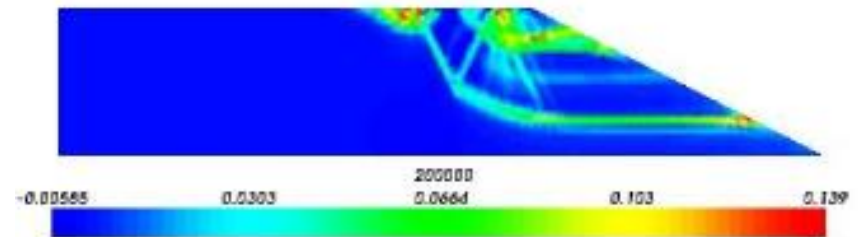


With 2d gradient

Plastic Volumic deformation in a dam modeling with 2d gradient (Foucault 2010) :



Coarse mesh



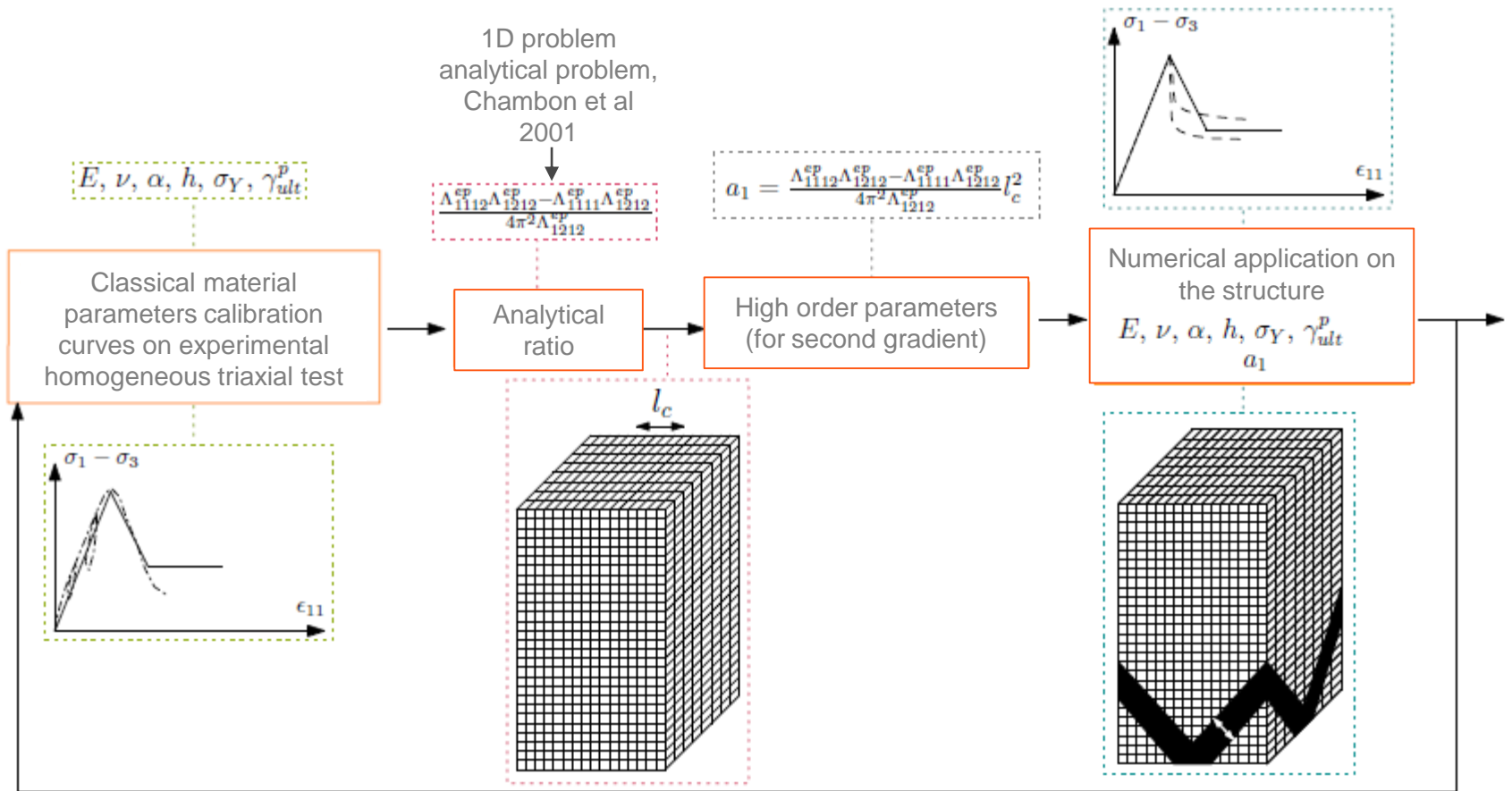
Fine mesh

Difficulty : Necessity of the introduction of additional parameters and internal length representative of localization pattern. A procedure is necessary

Mechanical laws and treatment (3/4)

Definition of a methodology to identify second gradient parameters
(Raude et al. 2015 – collaboration with GeoRessources)

=>Combination of a triaxial test modeling and analytical 1D solution



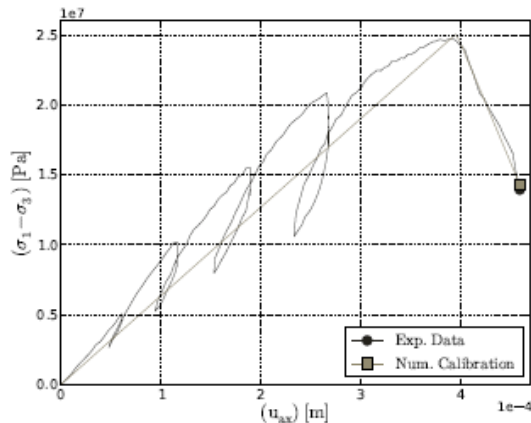
Change some classical material parameters (slope of the post peak branch)

Mechanical laws and treatment (4/4)

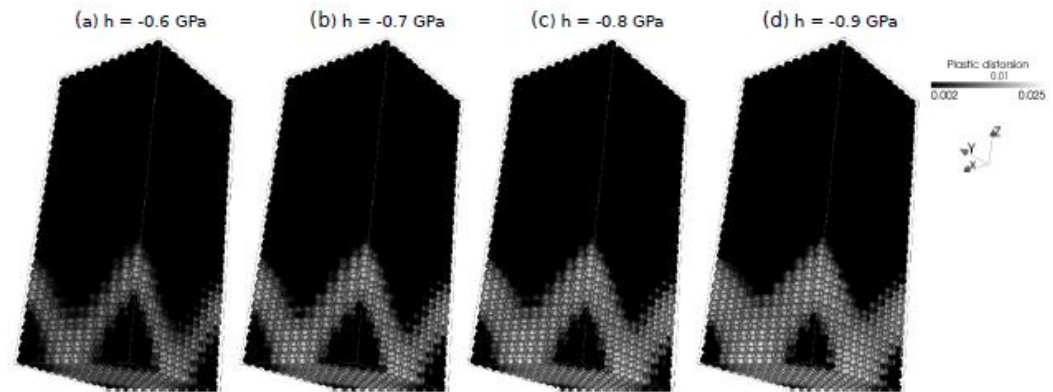
- Application to a shale specimen : Sisteron shale
 - Porous shale specimens from Sisteron : triaxial tests (GeoRessources)
 - Elasto-plastic law : Drucker Prager

⇒ *First hypothesis : we consider that characteristic length is about 1/3 of the horizontal size of the specimen*

First step : Calibration of the Drucker Prager parameters



Distribution of the accumulated plastic shear for different slopes for a fixed l_c



- Same results obtained with different meshes
- Perspective : Generalization of this method on different rocks and complex laws

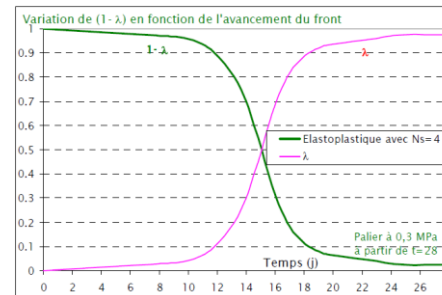
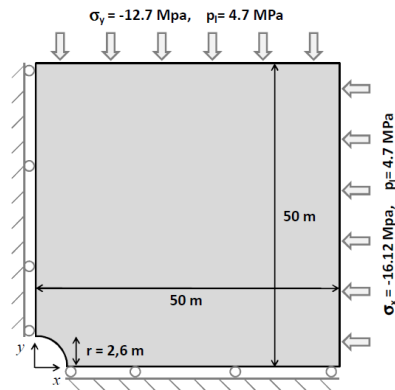
Mechanical Numerical simulations (1/3)

Context : Andra numerical benchmark exercise (Cuvilliez et al. 2014)

- Goal : compare numerical results of underground excavation to experimental measures (based on a realistic experiment of tunnel digging in Bure)
- Evaluate effect of HM couplings, concrete lining, etc.
- Data : geometry, advancement of digging, etc.

Computation hypothesis :

- 2D modeling using convergence-confinement method

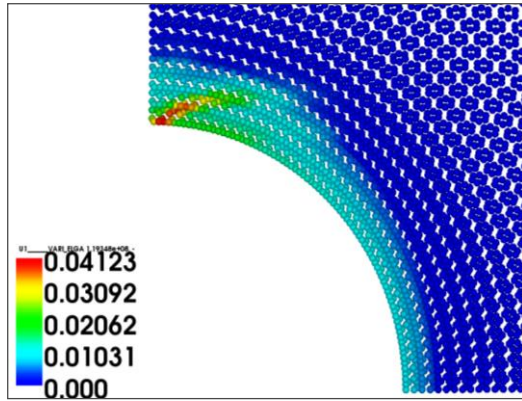


- Mechanical law : specific elasto-visco-plastic law (Laigle & Kleine)
- Coupling with hydraulic (HM simulation)
- Using of a regularization model

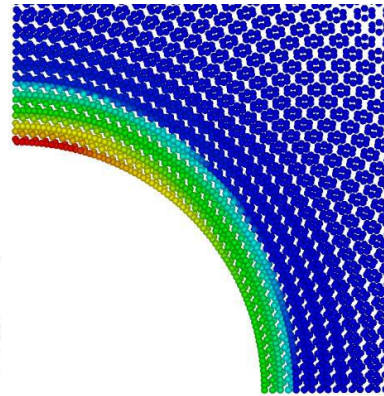
Mechanical Numerical simulations (2/3)

- Goal of regularization

Plastic strain hardening

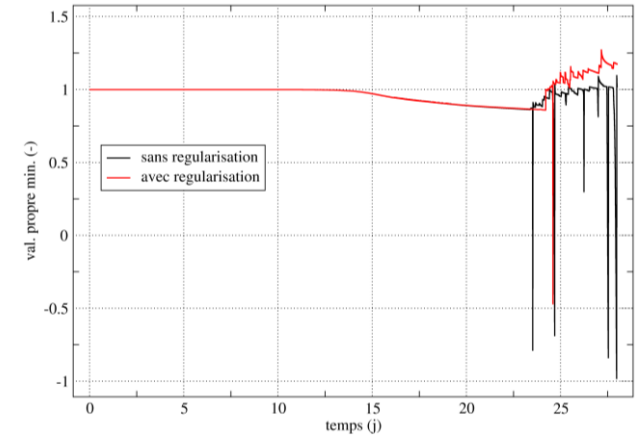


Local modeling

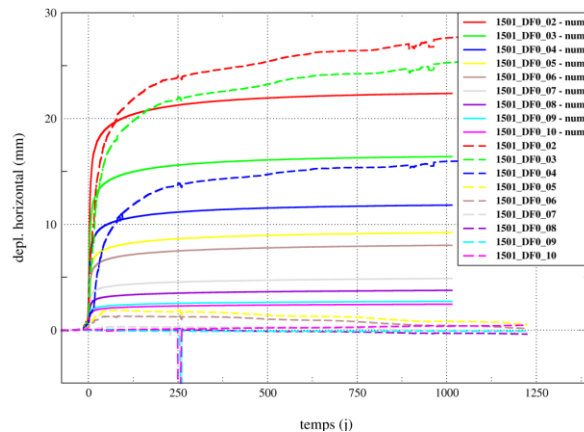


With regularization

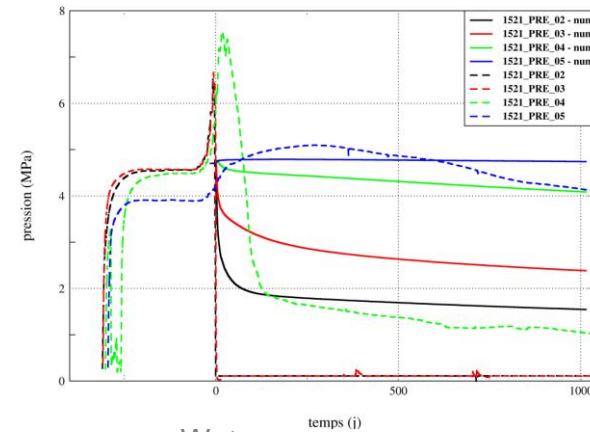
Eigenvalue evolution in Jacobian Matrix



- Comparison with experimental results



Vertical displacement



Water pressure

Mechanical Numerical simulations (3/3)

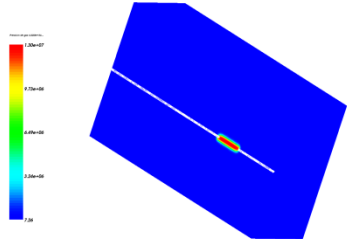
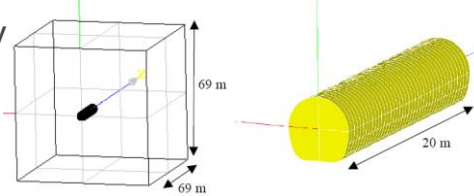
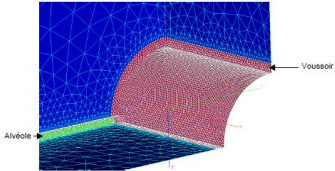
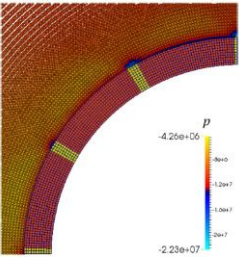
➤ Conclusion of Andra Benchmark simulation

- Numerical predictions are consistent with experimental results: water pressure drop and displacement well reproduced
- Necessity to have a coupling HM modeling even for displacement reproduction
- Necessity of non local method to avoid mesh dependency
- In the future 3D modeling will be necessary to reproduce correctly digging advancement (convergence confinement method is limited)



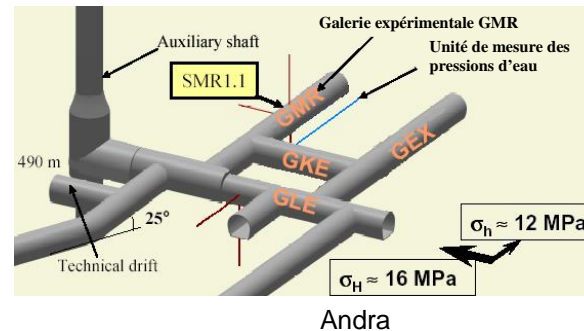
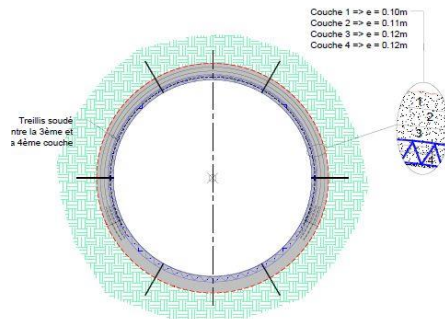
More complexity is required

What we can do (overview)

Geometry (example)	Mechanisms
<p>Ex : PGZ1 experiment modeling (FORGE Project) Injection of Hydrogen in anisotropic initially saturated host rock (Granet et al, 2010)</p> 	<p>HM (elastic) – two phase flow – several materials 3D ≈ 1 Millions DOF</p>
<p>Ex : Modeling of GMR Gallery (Meunier et al., 2011)</p> 	<p>HM (elastic)– realistic modeling of digging One material 3D ≈ 3 Millions DOF</p>
<p>Ex : 3D Modeling of High Activity cell 2015</p> 	<p>THM (viscoplastic law)– homogeneous digging 3D– 2d gradient ≈ 1 Millions DOF</p>
<p>Ex : 2D Modeling of a Gallery digging and concrete installation with compressible wedge and interface</p> 	<p>THM (viscoplastic) – 2d gradient – Simple modeling of digging (convergence confinement) – numerous heterogeneities 2D</p>

What we would like to do in the future

- 3D Viscoplastic THM study with digging progression on a complex geometry (crossing of galleries)



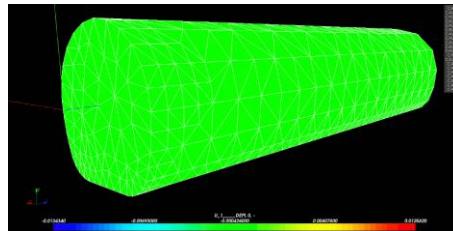
- 3D two-phase flow THM problem with several materials on a complex geometry

➔ Today : too expensive, too long

- More generally, we need :
 - More complexity (geometry, mechanisms, etc.) \Rightarrow more DOF and non linearities
 - More computations :
 - ✓ Sensitive analysis are required in order to reduce uncertainties
 - ✓ Experimental fitting

Numerical locks

- Very high non linear problems (mechanical laws, material parameters, etc.)
- Nature of the variables : multiple and heterogeneous
 - Convergence criterion difficult to define for Newton Method
 - Bad conditioning of Matrix => Iterative solvers not optimized
- Time evolution of Interest area
- Mesh refinement criterion well adapted to Hydro-Mechanical problem not yet available => explosion of DOF



HM (elastic) study of a digging. Using Homard mesh refinement tool (Meunier et al 2011)

Numerical perspectives

- Better use of iterative solvers (HPC problems) adapted to parallelism
- PHD Thesis, Rita Riedlbeck, 2014-2017 (supervised by D. di Pietro and A. Ern)
 - ✓ Stopping criteria and adaptative schemes for non linear Hydro-Mechanical problem (poroelasticity and poroplasticity)
 - ✓ Extension to poromechanical problem of a posteriori error estimates by equilibrated reconstructions of velocity and stress (Ern et Vohralik 2010). Flux equilibrium allows a systematic normalization.
 - ✓ Dominant error criterion for linear solvers
 - ✓ Dynamic adaptation of time and space step

Cf. Talk of Rita Riedlbeck tomorrow !

Conclusions and general perspectives

➤ **A Fully T.H.M tool with several possibilities in Code_Aster**

- More and more complexity : complex 3D structural problems, phenomena to take into account ... => HPC problems
- More and more sensitive computations are required in order to improve waste disposal dimensioning and robustness
- New model (Chemico-Hydro-Mechanical problems for bitumen swelling modeling – PHD thesis of G. Melot)

➤ **Link with experimental tests is crucial**

- Calibration of numerical tools (ex : characteristic length)
- Calibration of data
- More and more comparisons with experiments are required
- How to deal with dispersion of experimental data ? => uncertainties management will be a crucial issue