

# Volumetric expressions of the shape gradient of the compliance in structural shape optimization

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# Outline

- ① The linear elasticity equation
  - ▶ A problem in structural shape optimization
  - ▶ Surface and volumetric expressions of the shape gradient
  - ▶ The Boundary Variation Algorithm
- ② Minimization of the compliance under a volume constraint
  - ▶ Shape gradient using the pure displacement formulation
  - ▶ Shape gradient using a dual mixed variational formulation
  - ▶ A preliminary experimental comparison

# Outline

## 1 The linear elasticity equation

- A problem in structural shape optimization
- Surface and volumetric expressions of the shape gradient
- The Boundary Variation Algorithm

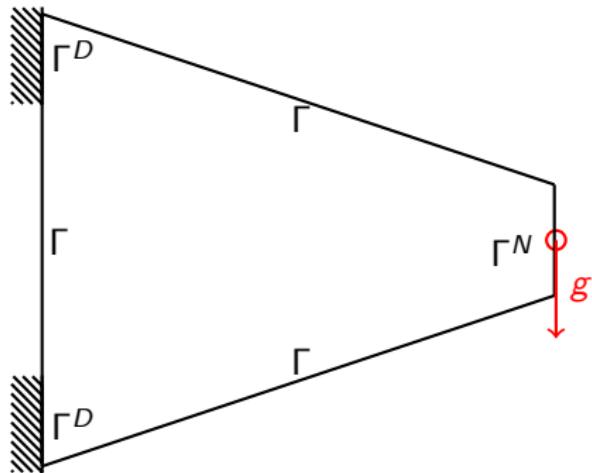
## 2 Minimization of the compliance under a volume constraint

- Shape gradient using the pure displacement formulation
- Shape gradient using a dual mixed variational formulation
- A preliminary experimental comparison

# The linear elasticity equation

- $\Omega \subset \mathbb{R}^d$  open connected domain;
- $\partial\Omega = \Gamma^N \cup \Gamma \cup \Gamma^D$ ,  $\mathcal{H}^{d-1}(\Gamma^D) > 0$ ;
- $\Gamma^N$ ,  $\Gamma$  and  $\Gamma^D$  are disjoint.

$$\begin{cases} -\nabla \cdot \sigma_\Omega = f & \text{in } \Omega \\ \sigma_\Omega = A e(u_\Omega) & \text{in } \Omega \\ \sigma_\Omega n = g & \text{on } \Gamma^N \\ \sigma_\Omega n = 0 & \text{on } \Gamma \\ u_\Omega = 0 & \text{on } \Gamma^D \end{cases}$$



Hooke's law for a linear elastic material:  $Ae(u_\Omega) = 2\mu e(u_\Omega) + \lambda \operatorname{tr}(e(u_\Omega)) \operatorname{Id}$

Compliance:

$$J(\Omega) := j(\Omega, \sigma_\Omega) = \int_{\Omega} A^{-1} \sigma_\Omega : \sigma_\Omega \, dx$$

# A problem in structural shape optimization

Minimization of the compliance under a volume constraint:  $\min_{\Omega \in \mathcal{U}_{ad}} J(\Omega)$

$\mathcal{U}_{ad} = \{\Omega \subset \mathbb{R}^d : \sigma_\Omega$  is the stress tensor fulfilling the linear elasticity equation  
on  $\Omega$  and  $V(\Omega) = |\Omega|$  is fixed $\}$ .

Gradient-based shape optimization:

# A problem in structural shape optimization

Minimization of the compliance under a volume constraint:  $\min_{\Omega \in \mathcal{U}_{ad}} J(\Omega)$

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 $\text{on } \Omega \text{ and } V(\Omega) = |\Omega| \text{ is fixed}\}.$

Gradient-based shape optimization:

---

Given the domain  $\Omega_0$ , set  $j=0$  and iterate:

1. Compute the solution of the state equation;
  2. Compute a descent direction  $\theta_j$  and an admissible step  $\mu_j$ ;
  3. Update the domain  $\Omega_{j+1} = (\text{Id} + \mu_j \theta_j) \Omega_j$ ;
  4. Until the stopping criterion is not fulfilled,  $j = j + 1$  and repeat.
-

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- 

## Classical optimization

$$\min_{x \in \mathbb{R}^n} f(x) \quad , \quad f : \mathbb{R}^n \rightarrow \mathbb{R}$$

Gradient-based descent direction  
in  $x$ :  $v$  s.t.  $(\nabla f(x), v) < 0$

$$x_{j+1} = x_j + \mu_j v_j$$

## Shape optimization

$$\min_{\Omega \in \mathcal{U}_{ad}} J(\Omega)$$

Gradient-based descent direction  
at  $\Omega$ :  $\theta$  s.t.  $\langle dJ(\Omega), \theta \rangle < 0$

$$\Omega_{j+1} = (\text{Id} + \mu_j \theta_j) \Omega_j$$

## Shape gradient

Let  $\theta \in X$  be an admissible smooth deformation of  $\Omega$ . The objective functional  $J$  is said to be  $X$ -differentiable at  $\Omega \in \mathcal{U}_{ad}$  if there exists a continuous linear form  $dJ(\Omega)$  on  $X$  such that  $\forall \theta \in X$  we have:

$$J((\text{Id} + \theta)\Omega) = J(\Omega) + \langle dJ(\Omega), \theta \rangle + o(\theta)$$

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## Surface expression

$$\langle dJ(\Omega), \theta \rangle = \int_{\partial\Omega} h_1(u_\Omega, \sigma_\Omega, \cdot) \theta \cdot n \ ds$$

## Volumetric expression

$$\langle dJ(\Omega), \theta \rangle = \int_{\Omega} h_2(u_\Omega, \sigma_\Omega, \cdot, \theta) \ dx$$

# Computing a descent direction

**Descent direction:**  $\theta$  such that  $\langle dJ(\Omega), \theta \rangle < 0$

Surface expression of the shape gradient:

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## The Boundary Variation Algorithm

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Given the domain  $\Omega_0$ , set  $\text{tol} > 0$ ,  $j = 0$  and iterate:

1. Compute the solution of the state equation;
  2. Compute the solution of the adjoint equation;
  3. Compute a descent direction  $\theta_j \in X$ ;
  4. Identify an admissible step  $\mu_j$ ;
  5. Update the domain  $\Omega_{j+1} = (\text{Id} + \mu_j \theta_j) \Omega_j$ ;
  6. While  $\langle dJ(\Omega_j), \theta_j \rangle > \text{tol}$ ,  $j = j + 1$  and repeat.
-

# Computing a descent direction

**Descent direction:**  $\theta$  such that  $\langle dJ(\Omega), \theta \rangle < 0$

Surface expression of the shape gradient:

$$\langle dJ(\Omega), \theta \rangle = \int_{\partial\Omega} h_1(u_\Omega, \sigma_\Omega, \cdot) \theta \cdot n \, ds \implies \theta = -h_1(u_\Omega, \sigma_\Omega, \cdot) n \text{ on } \partial\Omega$$

Volumetric expression of the shape gradient:

$$\langle dJ(\Omega), \theta \rangle = \int_{\Omega} h_2(u_\Omega, \sigma_\Omega, \cdot, \theta) \, dx \implies \theta = ?$$

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1. Compute the solution of the state equation;
  2. Compute the solution of the adjoint equation;
  3. Compute a descent direction  $\theta_j \in X$  s.t.  $(\theta_j, \delta\theta)_X + \langle dJ(\Omega_j), \delta\theta \rangle = 0 \quad \forall \delta\theta \in X$ ;
  4. Identify an admissible step  $\mu_j$ ;
  5. Update the domain  $\Omega_{j+1} = (\text{Id} + \mu_j \theta_j) \Omega_j$ ;
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# Minimization of the compliance under a volume constraint

We introduce a transformation  $X_\theta : \mathbb{R}^d \rightarrow \mathbb{R}^d$  and we define the open subset  $\Omega_\theta \subset \mathbb{R}^d$  as  $\Omega_\theta = X_\theta(\Omega)$  where  $\Gamma_\theta^N = X_\theta(\Gamma^N)$ ,  $\Gamma_\theta = X_\theta(\Gamma)$  and  $\Gamma_\theta^D = X_\theta(\Gamma^D)$ .

**Perturbation of the identity map:**  $X_\theta = \text{Id} + \theta + o(\theta)$  ,  $\theta \in W^{1,\infty}(\mathbb{R}^d; \mathbb{R}^d)$ .  
Jacobian of  $X_\theta$ :  $D_\theta = \text{Id} + \nabla \theta + o(\nabla \theta)$  ,  $I_\theta := \det D_\theta$

Under the assumption of a small perturbation  $\theta$ ,  $X_\theta$  is a diffeomorphism and belongs to the space

$$\mathcal{X} := \{X_\theta : (X_\theta - \text{Id}) \in W^{1,\infty}(\mathbb{R}^d; \mathbb{R}^d) \text{ and } (X_\theta^{-1} - \text{Id}) \in W^{1,\infty}(\mathbb{R}^d; \mathbb{R}^d)\}.$$

**Minimization of the compliance under a volume constraint:**  $\min_{\Omega_\theta \in \mathcal{U}_{ad}} J(\Omega_\theta)$

$\mathcal{U}_{ad} = \{\Omega_\theta : \exists X_\theta \in \mathcal{X}, \Omega_\theta = X_\theta(\Omega), \sigma_{\Omega_\theta}$  is the stress tensor fulfilling the linear elasticity equation on  $\Omega_\theta$  and  $V(\Omega_\theta) = |\Omega|\}$

$\Downarrow$

$$\boxed{\min_{\Omega_\theta \in \mathcal{U}_{ad}} L(\Omega_\theta) , \quad L(\Omega_\theta) = J(\Omega_\theta) + \gamma V(\Omega_\theta)}$$

# Minimization of the compliance under a volume constraint

We introduce a transformation  $X_\theta : \mathbb{R}^d \rightarrow \mathbb{R}^d$  and we define the open subset  $\Omega_\theta \subset \mathbb{R}^d$  as  $\Omega_\theta = X_\theta(\Omega)$  where  $\Gamma_\theta^N = X_\theta(\Gamma^N)$ ,  $\Gamma_\theta = X_\theta(\Gamma)$  and  $\Gamma_\theta^D = X_\theta(\Gamma^D)$ .

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$$\mathcal{X} := \{X_\theta : (X_\theta - \text{Id}) \in W^{1,\infty}(\mathbb{R}^d; \mathbb{R}^d)\}$$

The volume of  $\Omega_\theta$  is a purely geometrical quantity and does not depend on the solution of the state problem.

$$V(\Omega_\theta) = \int_{\Omega_\theta} dx_\theta = \int_{\Omega} I_\theta \, dx =: v(\theta)$$

$$\det(\text{Id} + C) = 1 + \text{tr}(C) + o(C)$$

$$\begin{aligned} \langle dV(\Omega), \theta \rangle &= \lim_{\theta \searrow 0} \frac{V(\Omega_\theta) - V(\Omega)}{\theta} \\ &= \lim_{\theta \searrow 0} \frac{v(\theta) - v(0)}{\theta} =: v'(0) \end{aligned}$$

↓

$$\min_{\Omega_\theta \in \mathcal{U}_{ad}} L(\Omega_\theta) , \quad L(\Omega_\theta) =$$

$$\langle dV(\Omega), \theta \rangle = \int_{\Omega} \nabla \cdot \theta \, dx = \int_{\partial\Omega} \theta \cdot n \, ds$$

# The pure displacement formulation

Data:  $f \in H^1(\mathbb{R}^d; \mathbb{R}^d)$ ,  $g \in H^2(\mathbb{R}^d; \mathbb{R}^d)$

Functional space for the variational formulation:

$$V_\Omega := H_{0,\Gamma^D}^1(\Omega; \mathbb{R}^d) = \{v \in H^1(\Omega; \mathbb{R}^d) : v = 0 \text{ on } \Gamma^D\}$$

State problem: We seek  $u_\Omega \in V_\Omega$  s.t.  $a_\Omega(u_\Omega, \delta u) = F_\Omega(\delta u) \quad \forall \delta u \in V_\Omega$

$$a_\Omega(u_\Omega, \delta u) := \int_\Omega A e(u_\Omega) : e(\delta u) \, dx \quad , \quad F_\Omega(\delta u) := \int_\Omega f \cdot \delta u \, dx + \int_{\Gamma^N} g \cdot \delta u \, ds.$$

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Compliance:

$$J(\Omega) = \int_\Omega A^{-1} \sigma_\Omega : \sigma_\Omega \, dx = \int_\Omega A e(u_\Omega) : e(u_\Omega) \, dx = \int_\Omega f \cdot u_\Omega \, dx + \int_{\Gamma^N} g \cdot u_\Omega \, ds$$

↓

$$J_1(\Omega_\theta) := - \min_{u_{\Omega_\theta} \in V_{\Omega_\theta}} \int_{\Omega_\theta} A e(u_{\Omega_\theta}) : e(u_{\Omega_\theta}) \, dx_\theta - 2 \int_{\Omega_\theta} f \cdot u_{\Omega_\theta} \, dx_\theta - 2 \int_{\Gamma_\theta^N} g \cdot u_{\Omega_\theta} \, ds_\theta =: j_1(\theta)$$

Shape gradient of the compliance:

$$\langle dJ_1(\Omega), \theta \rangle := \lim_{\theta \searrow 0} \frac{J_1(\Omega_\theta) - J_1(\Omega)}{\theta} = \lim_{\theta \searrow 0} \frac{j_1(\theta) - j_1(0)}{\theta} =: j'_1(0)$$

# Shape gradient using the pure displacement formulation

Transformation:  $\mathcal{P}_\theta : H_{0,\Gamma^D}^1(\Omega; \mathbb{R}^d) \rightarrow H_{0,\Gamma_\theta^D}^1(\Omega_\theta; \mathbb{R}^d)$  ,  $v_{\Omega_\theta} = \mathcal{P}_\theta(v_\Omega) = v_\Omega \circ X_\theta^{-1}$

## Lemma

Let  $u_\Omega \in H_{0,\Gamma^D}^1(\Omega; \mathbb{R}^d)$ . We consider  $u_{\Omega_\theta} = \mathcal{P}_\theta(u_\Omega)$ . It follows that

$$\frac{1}{2} \left( \nabla_{x_\theta} u_{\Omega_\theta} + \nabla_{x_\theta} u_{\Omega_\theta}^T \right) =: e_{x_\theta}(u_{\Omega_\theta}) = \frac{1}{2} \left( \nabla_x u_\Omega D_\theta^{-1} + D_\theta^{-T} \nabla_x u_\Omega^T \right)$$

where  $\nabla_{x_\theta}$  (respectively  $\nabla_x$ ) represents the gradient with respect to the coordinate of the deformed (respectively reference) domain.

## Compliance:

$$\begin{aligned} j_1(\theta) = & - \min_{u_\Omega \in V_\Omega} \int_\Omega A \left( \frac{1}{2} \left( \nabla u_\Omega D_\theta^{-1} + D_\theta^{-T} \nabla u_\Omega^T \right) \right) : \left( \frac{1}{2} \left( \nabla u_\Omega D_\theta^{-1} + D_\theta^{-T} \nabla u_\Omega^T \right) \right) I_\theta \, dx \\ & - 2 \int_\Omega f \circ X_\theta \cdot u_\Omega \, I_\theta \, dx - 2 \int_{\Gamma^N} g \circ X_\theta \cdot u_\Omega \, \text{Cof } D_\theta \, ds. \end{aligned}$$

# Shape gradient using the pure displacement formulation

**Transformation:**  $\mathcal{P}_\theta : H_{0,\Gamma^D}^1(\Omega; \mathbb{R}^d) \rightarrow H_{0,\Gamma_\theta^D}^1(\Omega_\theta; \mathbb{R}^d)$  ,  $v_{\Omega_\theta} = \mathcal{P}_\theta(v_\Omega) = v_\Omega \circ X_\theta^{-1}$

## Lemma

Let  $u_\Omega \in H_{0,\Gamma^D}^1(\Omega; \mathbb{R}^d)$ . We consider  $u_{\Omega_\theta} = \mathcal{P}_\theta$

$$\frac{1}{2} \left( \nabla_{x_\theta} u_{\Omega_\theta} + \nabla_{x_\theta} u_{\Omega_\theta}^T \right) =: e_{x_\theta}(u_{\Omega_\theta})$$

where  $\nabla_{x_\theta}$  (respectively  $\nabla_x$ ) represents the gradient in the deformed (respectively reference) domain.

We recall that  $X_\theta = \text{Id} + \theta + o(\theta)$ . Hence:

$$D_\theta = \text{Id} + \nabla \theta + o(\nabla \theta)$$

$$D_\theta^T = \text{Id} + \nabla \theta^T + o(\nabla \theta)$$

$$D_\theta^{-1} = \text{Id} - \nabla \theta + o(\nabla \theta)$$

$$\det(\text{Id} + C) = 1 + \text{tr}(C) + o(C)$$

$$\text{Cof}(\text{Id} + C) = \text{Id} + \text{tr}(C) \text{Id} - C + o(C)$$

## Compliance:

$$\begin{aligned} j_1(\theta) = & - \min_{u_\Omega \in V_\Omega} \int_\Omega A \left( \frac{1}{2} \left( \nabla u_\Omega D_\theta^{-1} + D_\theta^{-T} \nabla u_\Omega^T \right) \right) : \left( \frac{1}{2} \left( \nabla u_\Omega D_\theta^{-1} + D_\theta^{-T} \nabla u_\Omega^T \right) \right) I_\theta \, dx \\ & - 2 \int_\Omega f \circ X_\theta \cdot u_\Omega \, I_\theta \, dx - 2 \int_{\Gamma^N} g \circ X_\theta \cdot u_\Omega \, \text{Cof } D_\theta \, ds. \end{aligned}$$

**Shape gradient of the compliance** (By differentiating  $j_1(\theta)$  w.r.t  $\theta$  in  $\theta = 0$ ):

$$\begin{aligned} \langle dJ_1(\Omega), \theta \rangle = & \int_\Omega A e(u_\Omega) : \left( \nabla u_\Omega \nabla \theta + \nabla \theta^T \nabla u_\Omega^T \right) \, dx - \int_\Omega A e(u_\Omega) : e(u_\Omega)(\nabla \cdot \theta) \, dx \\ & + 2 \int_\Omega (\nabla f \theta \cdot u_\Omega + f \cdot u_\Omega (\nabla \cdot \theta)) \, dx + 2 \int_{\Gamma^N} (\nabla g \theta \cdot u_\Omega + g \cdot u_\Omega (\nabla \cdot \theta - \nabla \theta n \cdot n)) \, ds \end{aligned}$$

# A dual mixed formulation with weakly-enforced symmetry of the stress tensor

Functional spaces for the variational formulation:

$$H(\text{div}, \Omega; \mathbb{M}_d) := \{\tau \in L^2(\Omega; \mathbb{M}_d) : \nabla \cdot \tau \in L^2(\Omega; \mathbb{R}^d)\}$$

$$\Sigma_\Omega := \{\tau \in H(\text{div}, \Omega; \mathbb{M}_d) : \tau n = g \text{ on } \Gamma^N \text{ and } \tau n = 0 \text{ on } \Gamma\}$$

$$\Sigma_{\Omega,0} := \{\tau \in H(\text{div}, \Omega; \mathbb{M}_d) : \tau n = 0 \text{ on } \Gamma^N \cup \Gamma\}$$

$$V_\Omega := L^2(\Omega; \mathbb{R}^d), \quad Q_\Omega := L^2(\Omega; \mathbb{K}_d), \quad W_\Omega := V_\Omega \times Q_\Omega$$

**State problem:** We seek  $(\sigma_\Omega, (u_\Omega, \eta_\Omega)) \in \Sigma_\Omega \times W_\Omega$  such that

$$a_\Omega(\sigma_\Omega, \delta\sigma) + b_\Omega(\delta\sigma, (u_\Omega, \eta_\Omega)) = 0 \quad \forall \delta\sigma \in \Sigma_{\Omega,0}$$

$$b_\Omega(\sigma_\Omega, (\delta u, \delta\eta)) = F_\Omega(\delta u) \quad \forall (\delta u, \delta\eta) \in W_\Omega$$

$$a_\Omega(\sigma_\Omega, \delta\sigma) := \int_\Omega A^{-1} \sigma_\Omega : \delta\sigma \, dx$$

$$b_\Omega(\sigma_\Omega, (\delta u, \delta\eta)) := \int_\Omega (\nabla \cdot \sigma_\Omega) \cdot \delta u \, dx + \frac{1}{2\mu} \int_\Omega \sigma_\Omega : \delta\eta \, dx,$$

$$F_\Omega(\delta u) := - \int_\Omega f \cdot \delta u \, dx.$$

# Shape gradient using a dual mixed formulation I

Compliance:

$$J_3(\Omega_\theta) := \inf_{\sigma_{\Omega_\theta} \in \Sigma_{\Omega_\theta}} \sup_{(u_{\Omega_\theta}, \eta_{\Omega_\theta}) \in W_{\Omega_\theta}} \int_{\Omega_\theta} A^{-1} \sigma_{\Omega_\theta} : \sigma_{\Omega_\theta} \, dx_\theta + \int_{\Omega_\theta} (\nabla \cdot \sigma_{\Omega_\theta} + f) \cdot u_{\Omega_\theta} \, dx_\theta \\ + \frac{1}{2\mu} \int_{\Omega_\theta} \sigma_{\Omega_\theta} : \eta_{\Omega_\theta} \, dx_\theta =: j_3(\theta)$$

Mapping  $H(\text{div}, \Omega_\theta; \mathbb{M}_d)$  to  $H(\text{div}, \Omega; \mathbb{M}_d)$

A key aspect of this transformation is the preservation of the normal traces of the tensors under analysis.  $\implies$  Special isomorphism known as **contravariant Piola transform**.

Transformations:

$$\mathcal{Q}_\theta : H(\text{div}, \Omega; \mathbb{M}_d) \rightarrow H(\text{div}, \Omega_\theta; \mathbb{M}_d) \quad , \quad \tau_{\Omega_\theta} = \mathcal{Q}_\theta(\tau_\Omega) = \frac{1}{I_\theta} D_\theta \tau_\Omega \circ X_\theta^{-1} D_\theta^T$$
$$\mathcal{R}_\theta : L^2(\Omega; \mathbb{R}^d) \rightarrow L^2(\Omega_\theta; \mathbb{R}^d) \quad , \quad v_{\Omega_\theta} = \mathcal{R}_\theta(v_\Omega) = D_\theta^{-T} v_\Omega \circ X_\theta^{-1}$$

Lemma

Let  $\sigma_\Omega \in H(\text{div}, \Omega; \mathbb{M}_d)$ . We consider  $\sigma_{\Omega_\theta} = \mathcal{Q}_\theta(\sigma_\Omega)$ . It follows that

$$\nabla_{x_\theta} \cdot \sigma_{\Omega_\theta} = \frac{1}{I_\theta} D_\theta \nabla_x \cdot \sigma_\Omega$$

where  $\nabla_{x_\theta} \cdot$  (respectively  $\nabla_x \cdot$ ) represents the divergence with respect to the coordinate of the deformed (respectively reference) domain.

## Shape gradient using a dual mixed formulation II

Compliance:

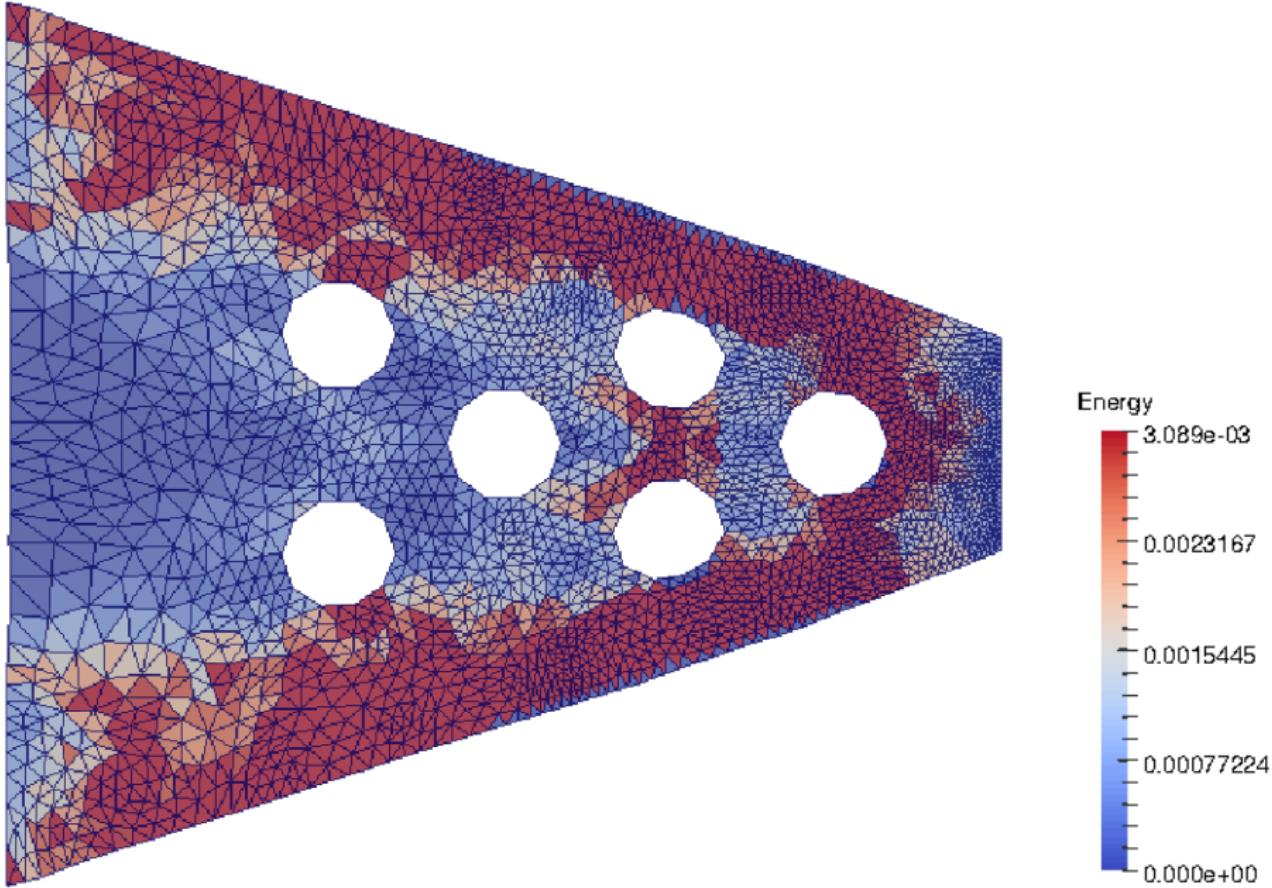
$$\begin{aligned} j_3(\theta) = & \inf_{\sigma_\Omega \in \Sigma_\Omega} \sup_{(u_\Omega, \eta_\Omega) \in W_\Omega} \frac{1}{2\mu} \int_\Omega \frac{1}{l_\theta} D_\theta^T D_\theta \sigma_\Omega D_\theta^T D_\theta : \sigma_\Omega \, dx \\ & - \frac{\lambda}{2\mu(d\lambda + 2\mu)} \int_\Omega \frac{1}{l_\theta} \operatorname{tr}(D_\theta^T D_\theta \sigma_\Omega) \operatorname{tr}(D_\theta^T D_\theta \sigma_\Omega) \, dx \\ & + \frac{1}{2\mu} \int_\Omega \frac{1}{l_\theta} D_\theta^T D_\theta \sigma_\Omega D_\theta^T D_\theta : \eta_\Omega \, dx \\ & + \int_\Omega (\nabla \cdot \sigma_\Omega) \cdot u_\Omega \, dx + \int_\Omega f \circ X_\theta \cdot (D_\theta^{-T} u_\Omega) l_\theta \, dx. \end{aligned}$$

Shape gradient of the compliance:

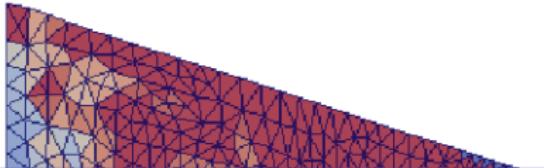
$$\begin{aligned} \langle dJ_3(\Omega), \theta \rangle = & \frac{1}{2\mu} \int_\Omega (N(\theta) \sigma_\Omega : \sigma_\Omega + \sigma_\Omega N(\theta) : \sigma_\Omega) \, dx \\ & - \frac{\lambda}{2\mu(d\lambda + 2\mu)} \int_\Omega 2 \operatorname{tr}(N(\theta) \sigma_\Omega) \operatorname{tr}(\sigma_\Omega) \, dx \\ & + \frac{1}{2\mu} \int_\Omega (N(\theta) \sigma_\Omega : \eta_\Omega + \sigma_\Omega N(\theta) : \eta_\Omega) \, dx \\ & + \int_\Omega \left( \nabla f \theta \cdot u_\Omega + f \cdot u_\Omega (\nabla \cdot \theta) - f \cdot (\nabla \theta^T u_\Omega) \right) \, dx, \end{aligned}$$

$$\text{where } N(\theta) := \nabla \theta + \nabla \theta^T - \frac{1}{2} (\nabla \cdot \theta) \operatorname{Id}.$$

# A cantilever with six holes ( $V_0 = 40.59$ , $\gamma_0 = 0.13$ )



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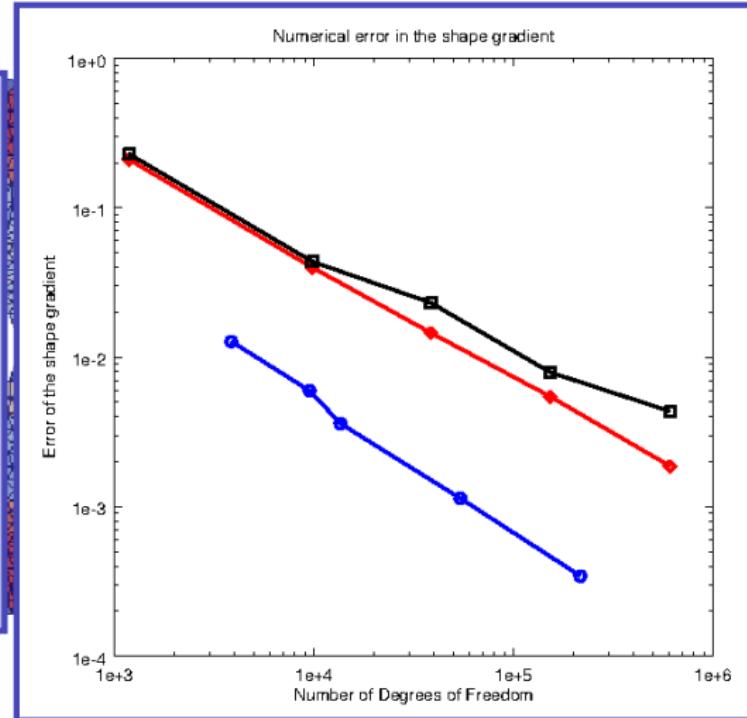
Finite Element spaces  
for the discretization

## Pure displacement formulation

- Displacement field:  $\mathbb{P}^1 \times \mathbb{P}^1$
- In black: surface expression
- In red: volumetric expression

## Dual mixed formulation

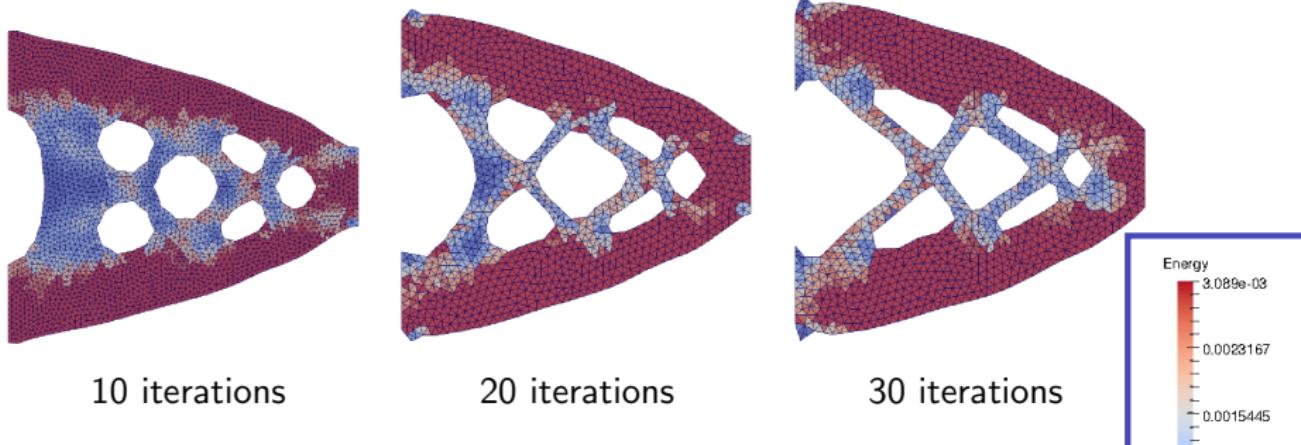
- Stress tensorfield:  $BDM_1 \times BDM_1$
- Displacement field:  $\mathbb{P}^0 \times \mathbb{P}^0$
- Lagrange multiplier:  $\mathbb{P}^0$
- In blue: volumetric expression



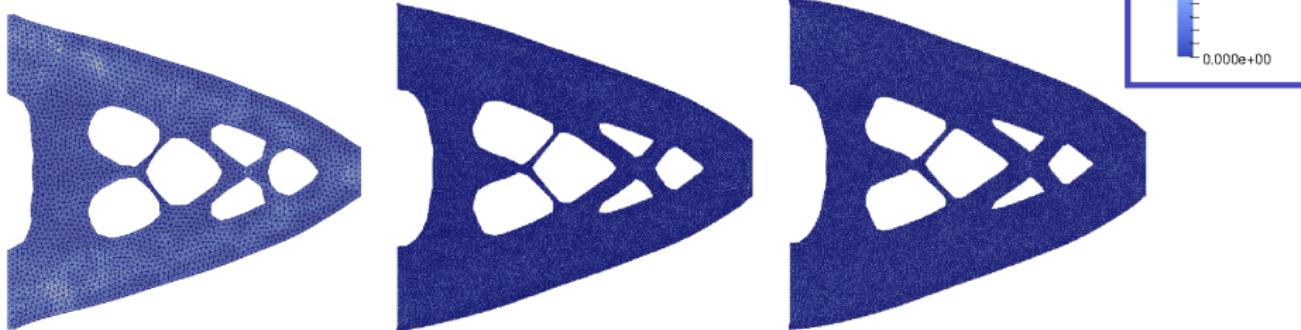
0.000e+00

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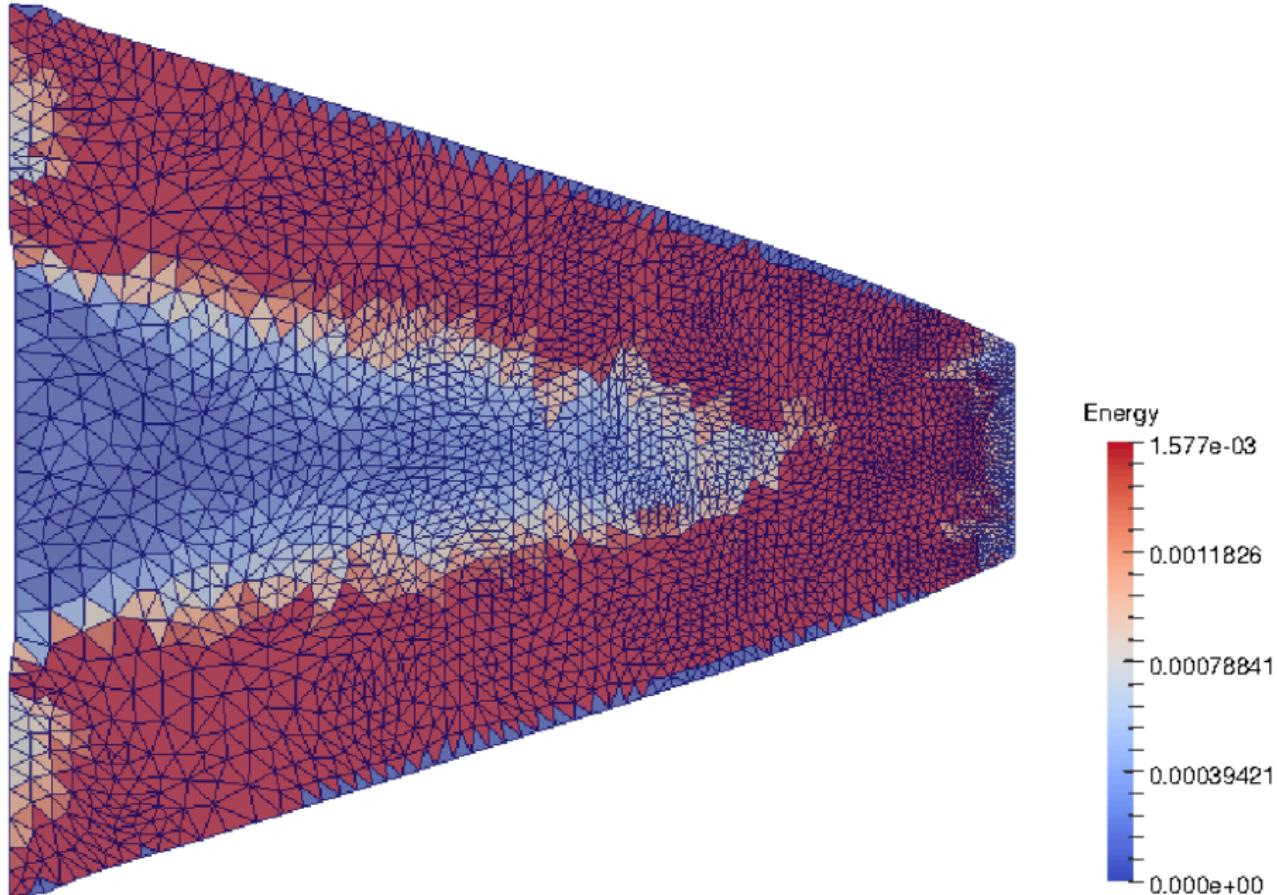
Pure displacement formulation:



Dual mixed formulation:

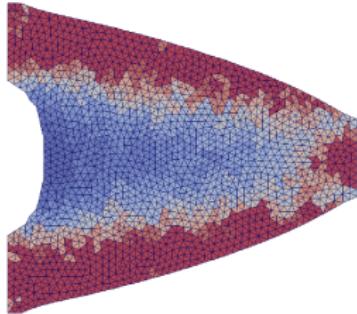


# A bulky cantilever ( $V_0 = 45$ , $\gamma_0 = 0.1$ )

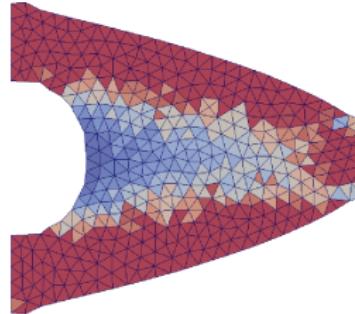


# A bulky cantilever ( $V_0 = 45$ , $\gamma_0 = 0.1$ )

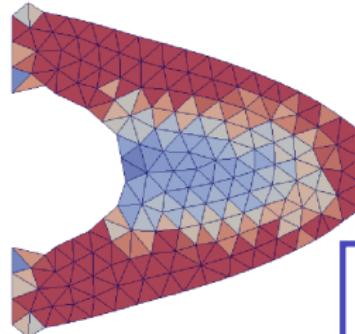
Pure displacement formulation:



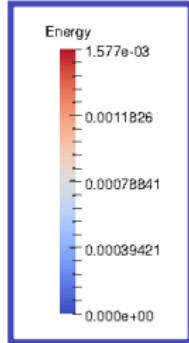
10 iterations



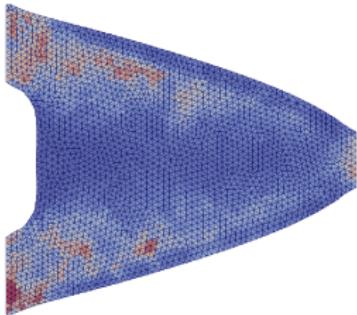
20 iterations



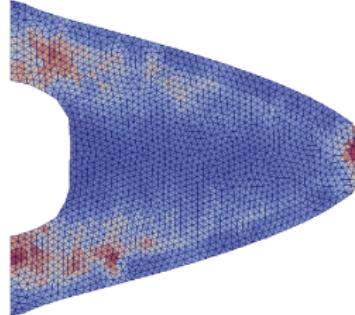
30 iterations



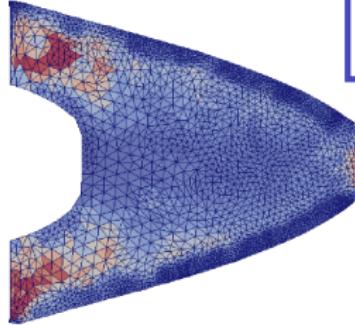
Dual mixed formulation:



M. Giacomini



Volumetric shape gradient

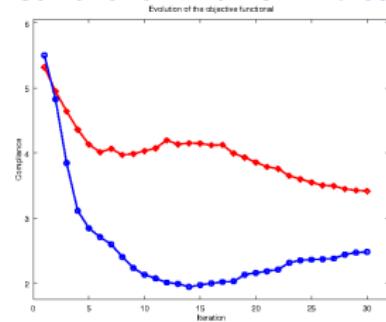


October 6 2016 (IHP)

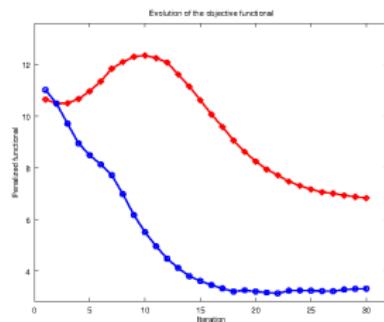
# A preliminary experimental comparison

Pure displacement (in red) VS dual mixed (in blue) formulations

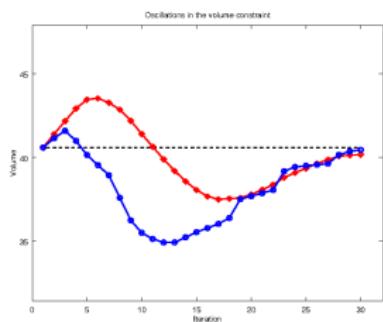
## Cantilever with six holes:



$$J(\Omega)$$

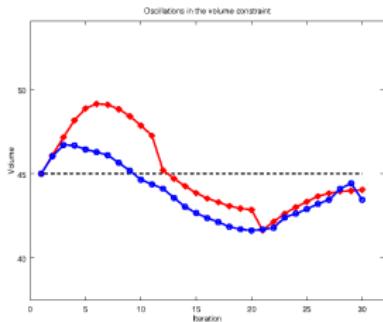
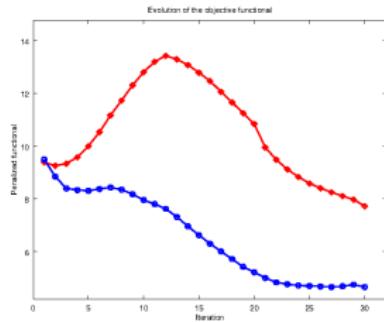
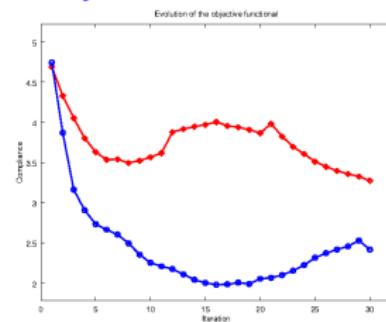


$$L(\Omega) = J(\Omega) + \gamma V(\Omega)$$



$$V(\Omega)$$

## Bulky cantilever:



# Conclusions

From the experimental results:

- Better convergence rate using the volumetric shape gradient.
- More robust approach using the dual mixed formulation of the problem.
- Configurations with lower compliance (and elastic energy) are obtained starting from the dual mixed formulation.
- The dual mixed formulation seems to provide better convergence rate than the pure displacement one.

Ongoing and future investigations:

- Proof of the equivalence of the volumetric expressions in the continuous framework
- A priori estimate of the error due to the numerical approximation of the shape gradient